

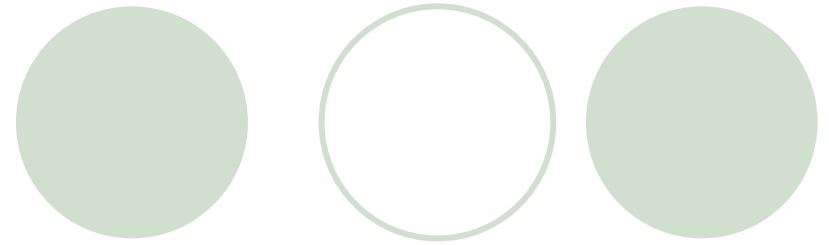
Positron Propelled and Powered Space Transport Vehicle for Planetary Missions

Positronics Research, LLC, Santa Fe, NM

Work performed under
Universities Space Research Association
Research Subaward No. 07605-003-048

Presented at NIAC Phase I Fellows Meeting
Atlanta, GA, March 7-8, 2006

Team Members



- Dr. Gerald Smith – Principal Investigator
- Dr. John Metzger – Consultant
- Mr. Kirby Meyer – Engineer
- Dr. Les Thode – Physicist

Mars Missions Require Large Payload Masses and Significant ΔV s to Reduce Radiation Exposure

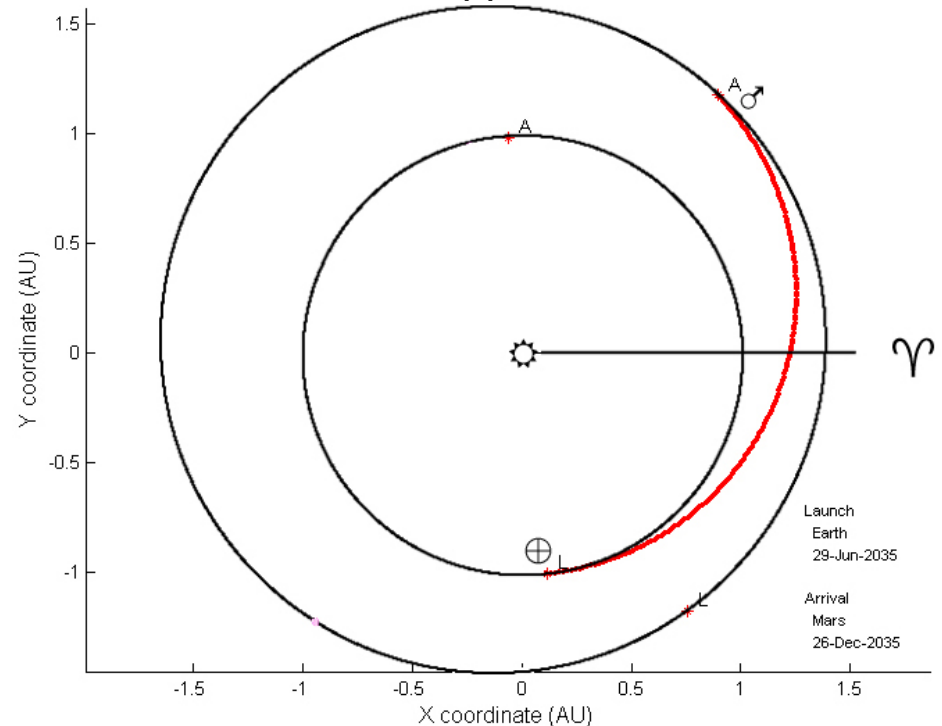
- Studies* suggested payloads of 60,000 kg.
- Orbital mechanics suggest $\Delta V = 3.7$ km/sec for 6-month, one-way transit to Mars.

- Rocket equation:

$$\Delta V = u_{eq} \ln\left(\frac{M_o}{M_b}\right) \cong I_{sp} g \cdot \ln\left(\frac{M_o}{M_b}\right)$$

- Assuming 40,000 kg for tank and engine, a chemical system to Mars could be 250,000 kg!
- Apollo payload ~44,000 kg. Result: Massively complex staged system, expensive.

A 2035, Earth-Mars Opposition Mission Scenario



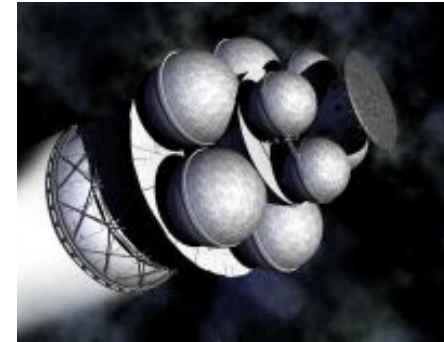
*B.G. Drake, ed. "Reference Mission Version 3.0: Addendum to the Human Exploration of Mars: The Reference Mission of the NASA Mars Exploration Study Team," <http://ares.jsc.nasa.gov/HumanExplore/Exploration/EXLibrary/docs/MarsRef/addendum/index.htm>, June 1998.

Studies Suggested $I_{sp} > 1000$ sec to Reduce System Weights

- High I_{sp} , high thrust system limits propulsion types to:
 1. Nuclear-thermal (NERVA/Rover).
 2. Fusion (e.g. Daedalus).
 3. Antimatter.
 4. Combinations of above.

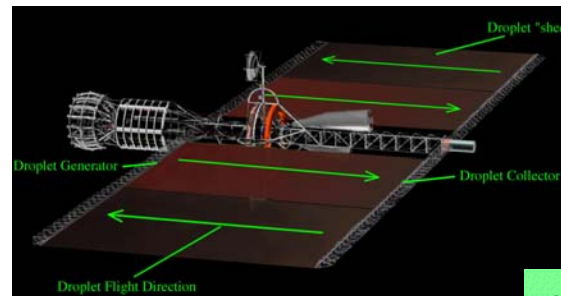


Nuclear-thermal, NASA GRC



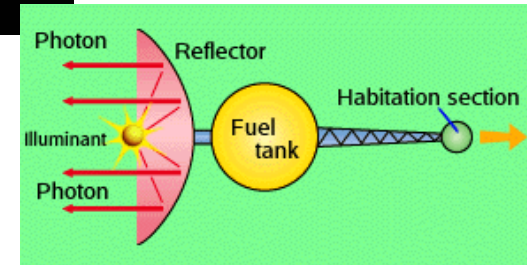
Daedalus

(<http://www.aemann.pwp.blueyonder.co.uk/>)



ICAN Antiproton-Catalyzed Microfission/Fusion (ACMF), PSU.

Direct positrons (Sänger)
(<http://spectech.bravepages.com>)

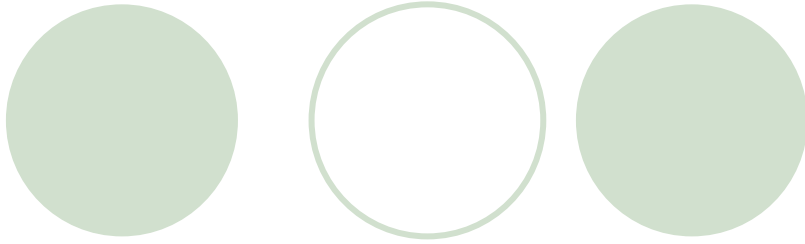


Propulsion	I_{sp} (sec)
Nuclear-thermal	800-3000
Fusion	$10^4 - 10^5$
Hybrid antimatter fusion	13,000
Direct positrons	10^7

Why Positrons?

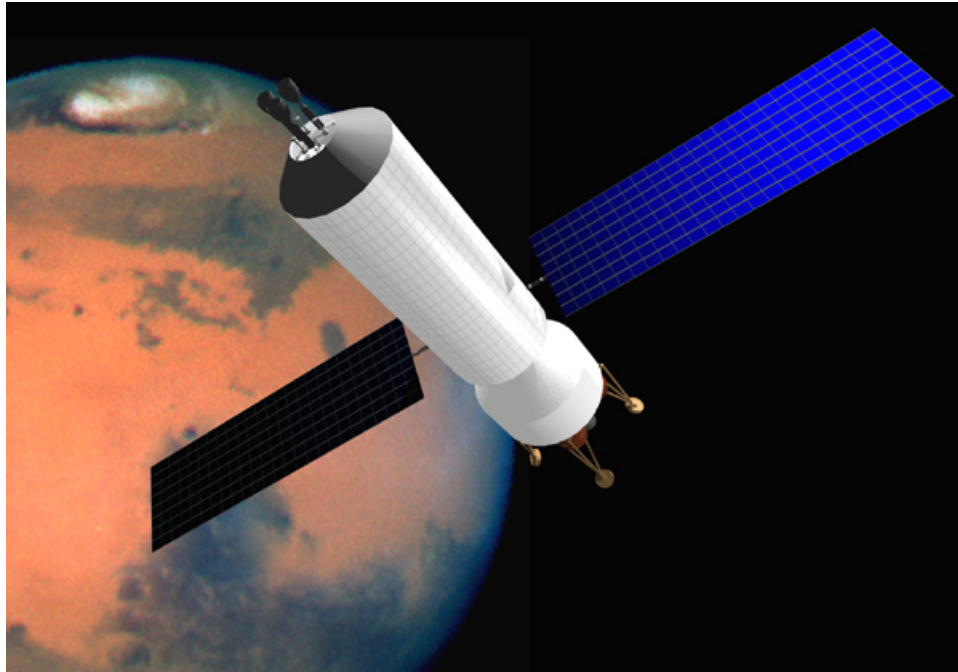
- Antimatter has highest specific energy in existence.
- No residual radiation.
- Large amounts can be made available.
- Promising storage developments.**
- We estimate approximately 4 mg of positrons for a one-way trip to Mars with a system mass of 100,000 kg (e+ not used for powering payload).

**discussion restricted under provisions of AFRL contract #F08630-02-C-0018



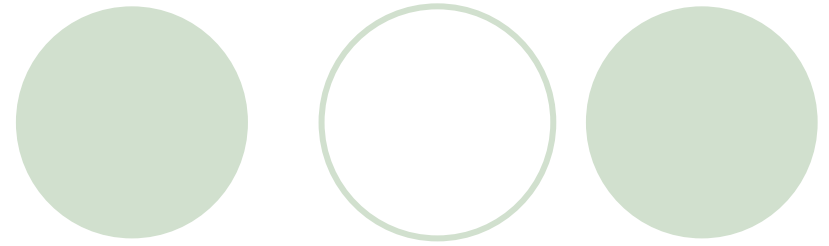
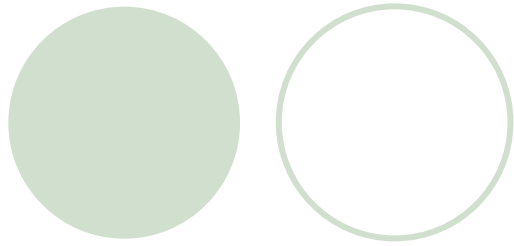
Propulsion Type	Specific Energy (MJ/kg)
Chemical LO ₂ /LH ₂ Atomic H	10 400
Fission	8×10^6
Fusion	3×10^8
Antimatter	1.8×10^{11}

Goal: Investigate Candidate Systems That Can Use Positrons



PRLLC solid-core spacecraft

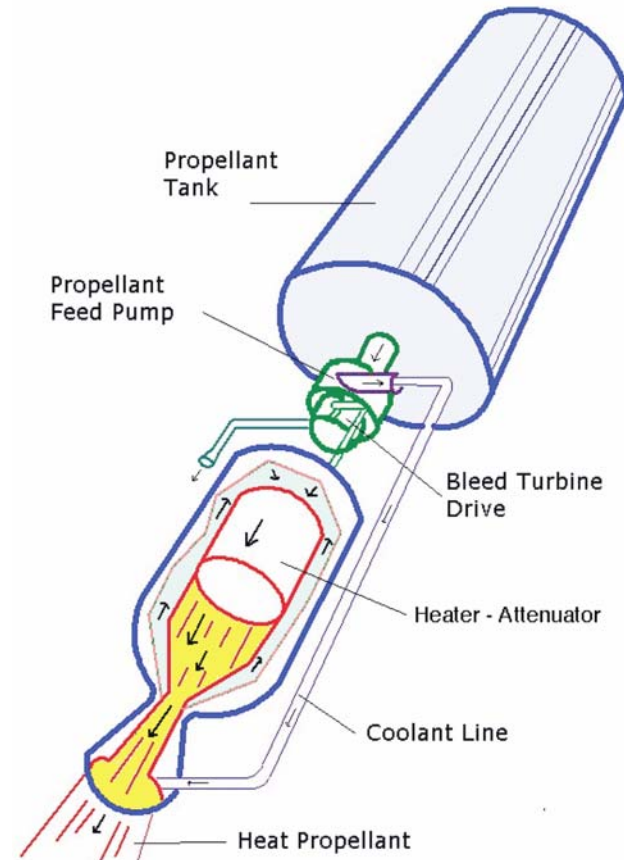
- Positron-electron annihilations create two, 511 keV gamma rays.
 - Last positron concept developed by Eugen Sänger, 1935. Reflected gamma rays created thrust.
 - There is presently no means to reflect gamma rays. They must be used to heat another propellant.
 - Goal: delineate properties of positron-driven engine for fast access to Mars.
1. **Solid Core.**
 2. **Gas Core.**
 3. **Other concepts.**



Solid-Core Engine and Power Systems

Positron Solid-Core Energy Source

- Flexible for both propulsion & power
- Outstanding performance capability
 - High I_{sp} , ~1000 sec, propulsion.
 - High thrust, comparable to chemical & nuclear-thermal engines.
 - High specific mass systems (P/M or T/W).
- Not an operating or shutdown radiation source
 - No shielding required.
 - Does not need to be separated from Crew/Payload.
 - No shutdown cooling required.
- Simple operation
 - On-Off operation.
 - No complex control mechanisms.
 - No criticality requirements.
- Nearer-term than other hi-tech options.

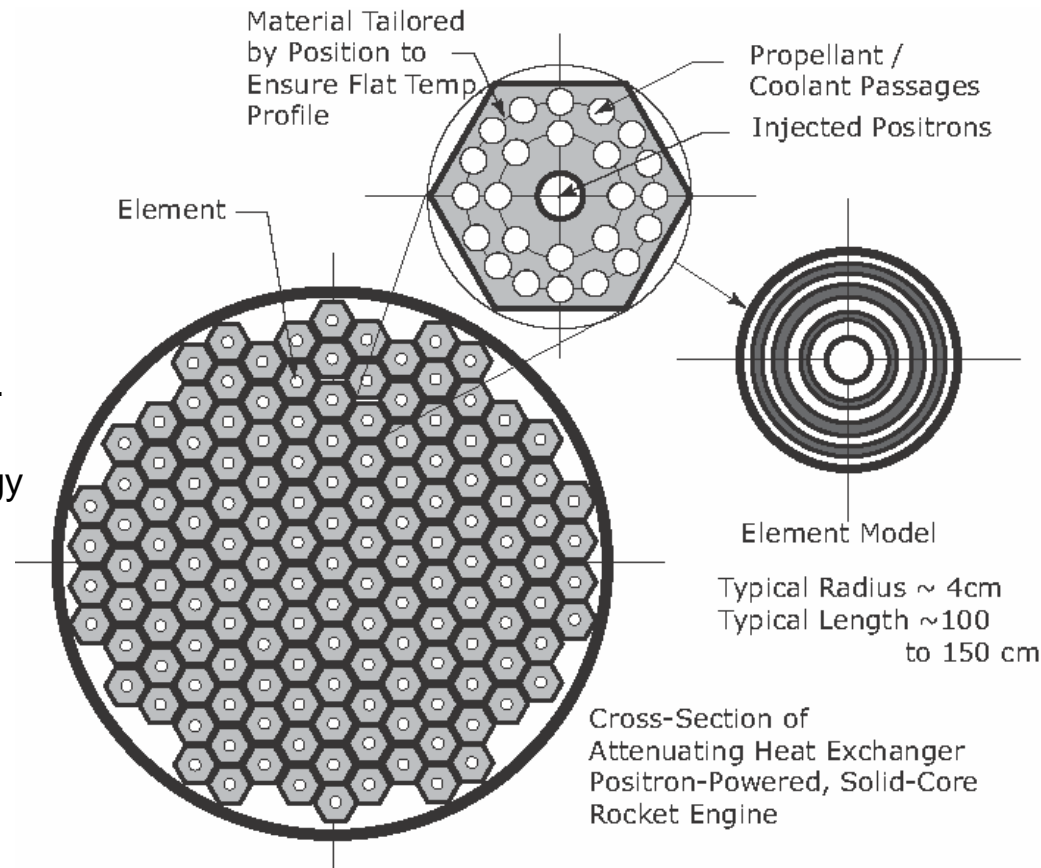


Positron-Powered Rocket Engine
Modified from Experienced Gained from the Space Nuclear
Program (Rover); LA-10062-H, D.R. Koenig May 1986

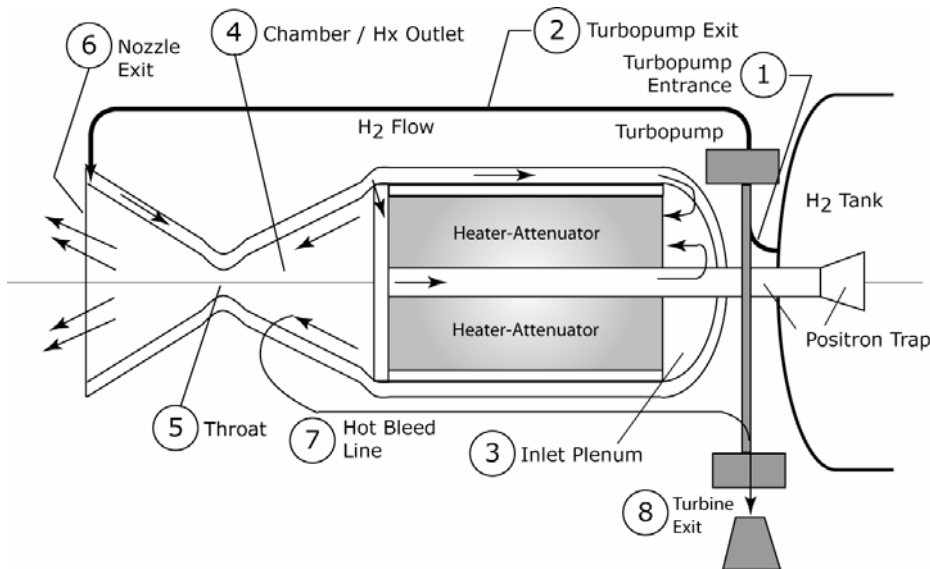
Positron Heater-Attenuator

The Energy Source of a Positron-Powered System

- Similar in arrangement to NERVA/Rover configuration
 - Hexagonal elements appropriately supported for structural & vibration considerations.
 - Flow channels orificed to preclude viscosity instability.
- Element configuration
 - Central channel for positron injection.
 - Propellant/coolant channels.
 - Materials tailored to ensure flat energy profile; i.e., flat exit propellant temperature profile.
- Element model
 - Concentric annular shells.
- Power & material temperature determine number & geometry of elements.



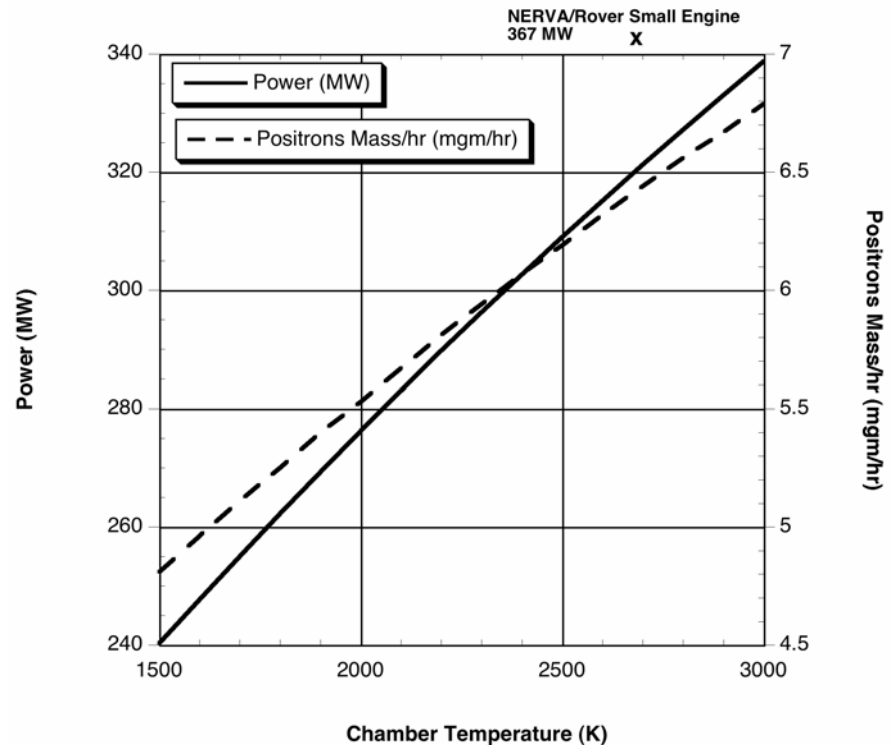
Thermal-Fluids Rocket Engine Model



- A thermal-fluids model for concept analysis
 - Hot-bleed cycle.
 - Determines temp., pressure, & enthalpy at every point indicated.
 - Determines engine performance - thrust, I_{sp} , power, nozzle geometry.
 - Determines e+ utilization (number and mass rates) and propellant utilization.
 - Estimates turbopump requirements.
 - Estimates ΔP thru heater-attenuator.
 - Dependant upon geometry of attenuator-heater.
- Model based on thermodynamic principals, energy balance and momentum balance.

Solid-Core Positron Rocket Results

- Analyzed two classes of rocket engines
 - Small engines - 72 kN (16k lb_f) thrust.
 - Large engines - 1000 kN (225k lb_f).
 - Results base-lined to results from NERVA/Rover.
- Results of analysis comparable to NERVA / Rover published results.*
- Geometry optimized for material surface temperatures up to 3000 K.

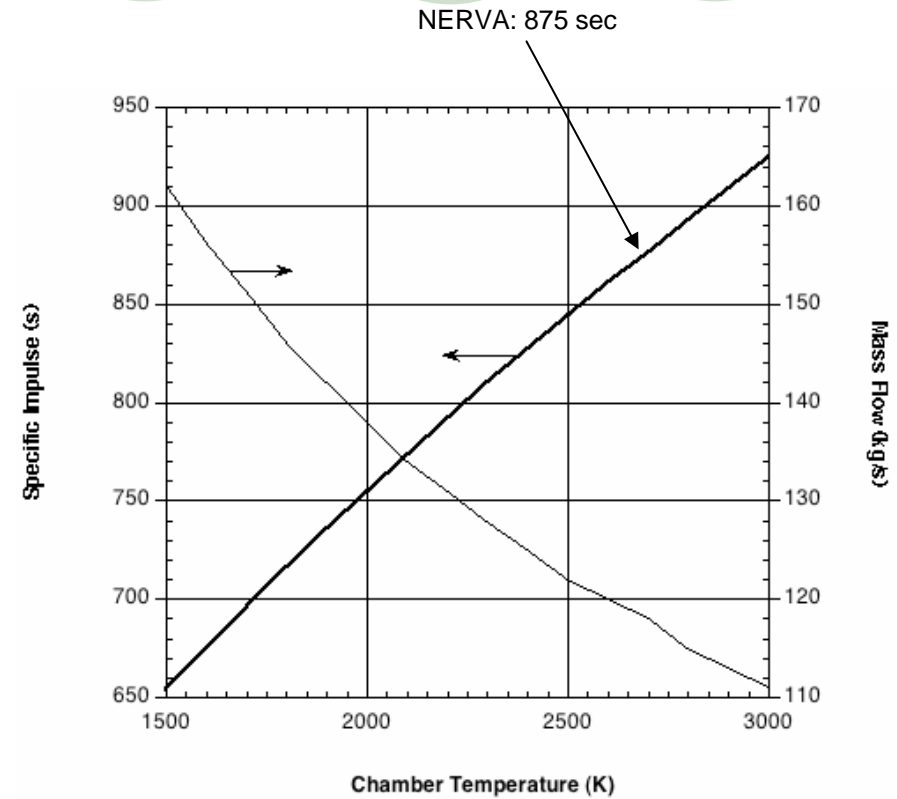
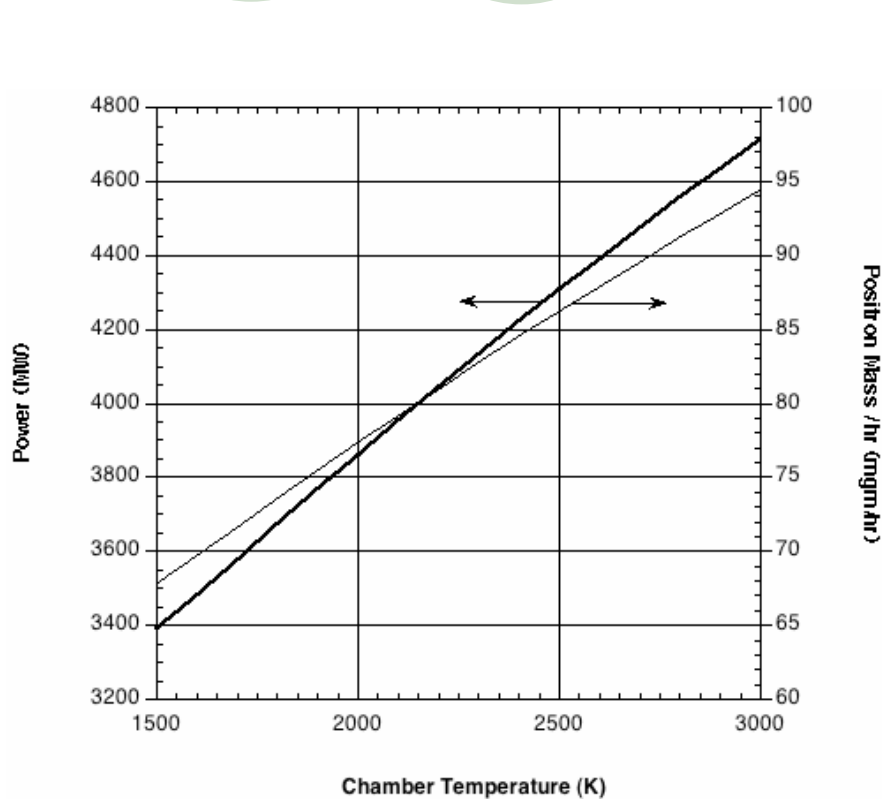


Small Engine (72 kN) Results

*Daniel R. Koenig, "Experience Gained from the Space Nuclear Rocket Program (Rover)," Los Alamos National Laboratory report LA-10062-H, May 1986

Solid-Core Positron Rocket Results

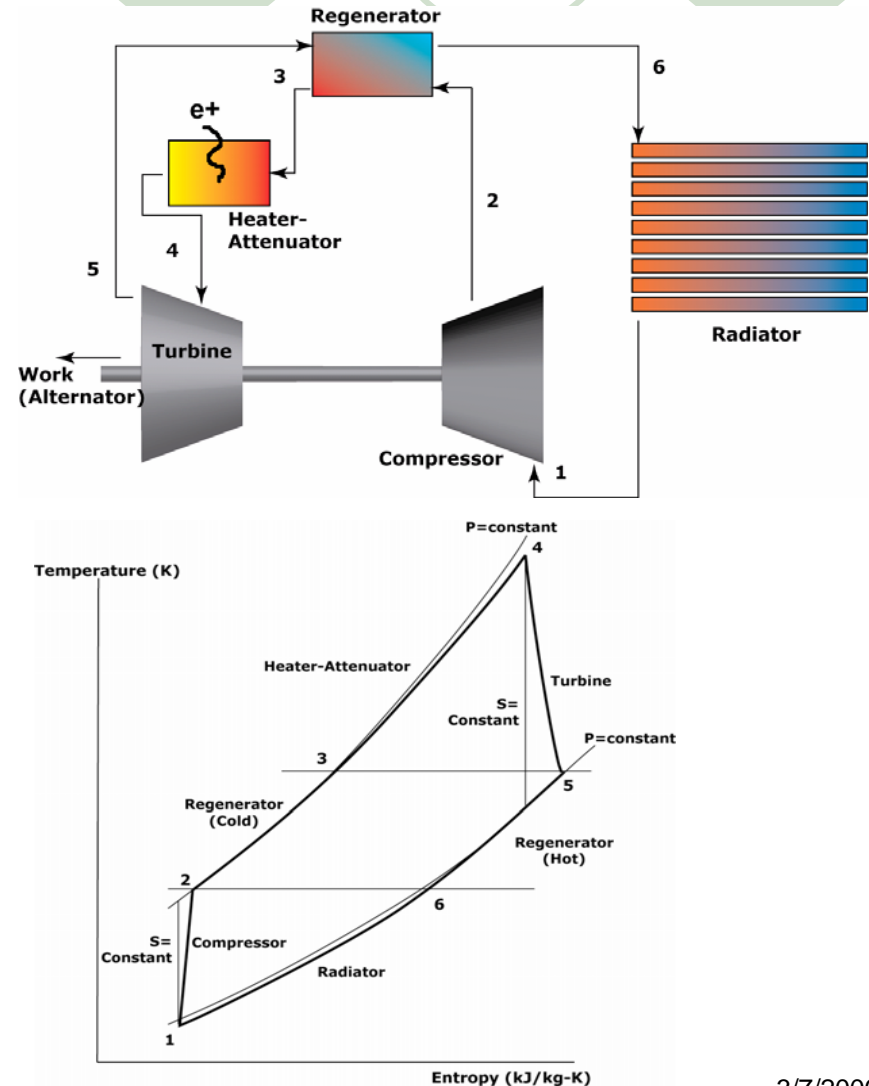
(continued)



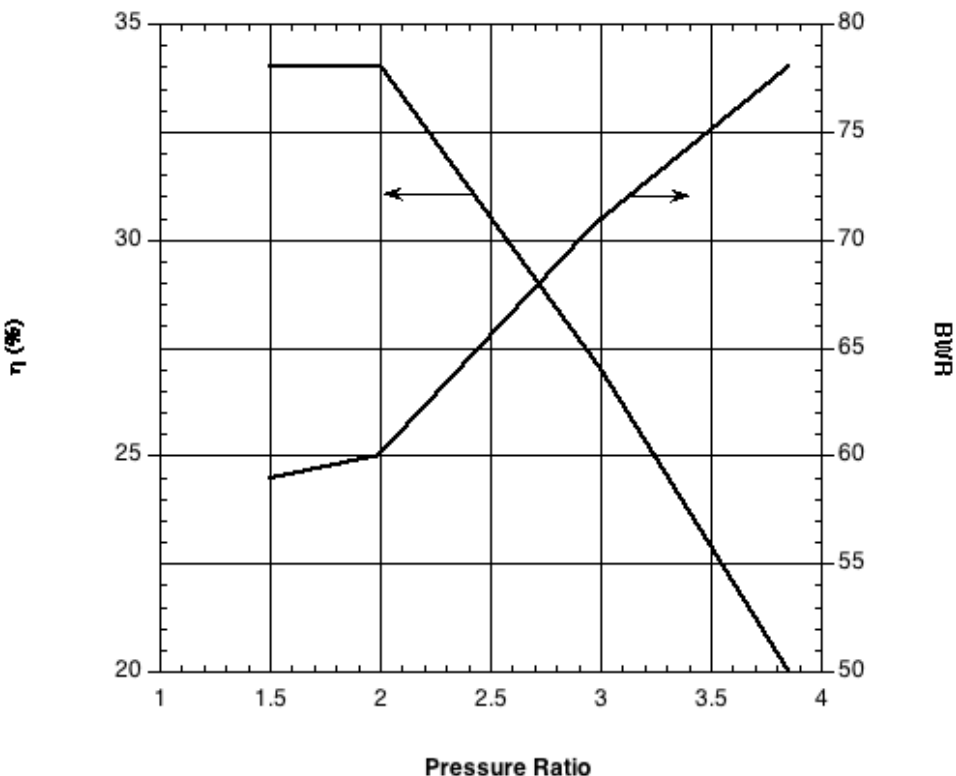
Large engine (100 kN) results. Specific impulse graph matches that for small engine.

Closed Brayton Cycle (CBC) Model Using Positrons for Power Plant and/or Martian Surface

- A thermal-fluids model for concept analysis
 - Variable He-Xe mixtures and compressor/turbine pressure ratio.
 - Regeneration (allows for 2-stage w/ reheat and inter-cooling).
 - Determines temp., pressure, & enthalpy at every point indicated.
 - Determines cycle performance - efficiency and back-work ratio.
 - Estimates radiator size, regenerator size and heater-attenuator material temperatures.
 - Determines e^+ utilization (number and mass rates).
 - Estimates ΔP thru heater-attenuator.
 - Dependant upon geometry of attenuator-heater.
- Model based on thermodynamic principles, energy balance and momentum balance.



Solid-Core Positron CBC Results



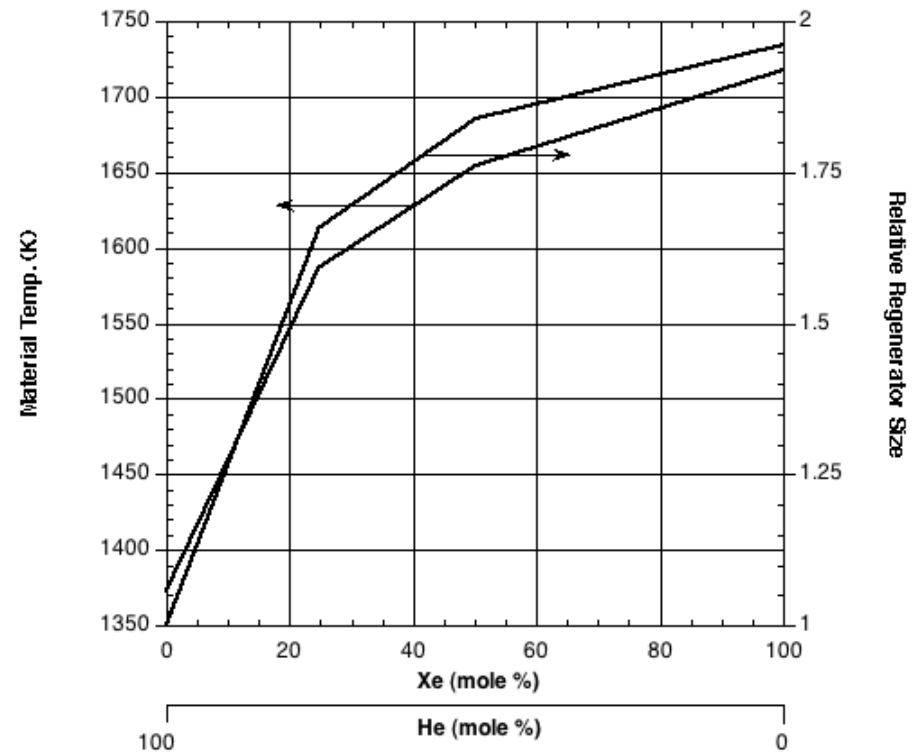
Expect about 30% efficiency, 7 $\mu\text{g/hr}$

- Results are for 100 kW_e available system power.
 - Example: Efficiency of 25% means 400 kW of e⁺ power necessary for 100 kW output.
- Selection of pressure ratio is a trade-off of system mass and efficiency.
 - Efficiency decreases with pressure ratio.
 - Back-work ratio (BWR) increases.

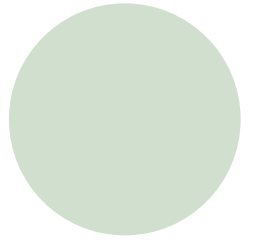
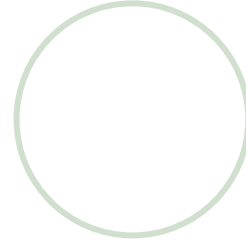
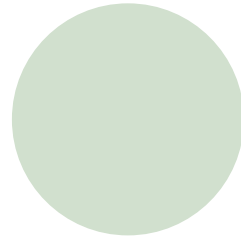
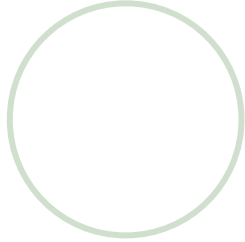
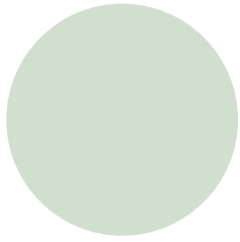
Solid-Core Positron CBC Results

(continued)

- Some performance parameters are also dependent on He-Xe ratio (density and molecular weight)
 - Material temperature
 - Component sizes
- Optimal near He = 72%.
- Lower desired temperatures mean lighter materials such as titanium can be used.



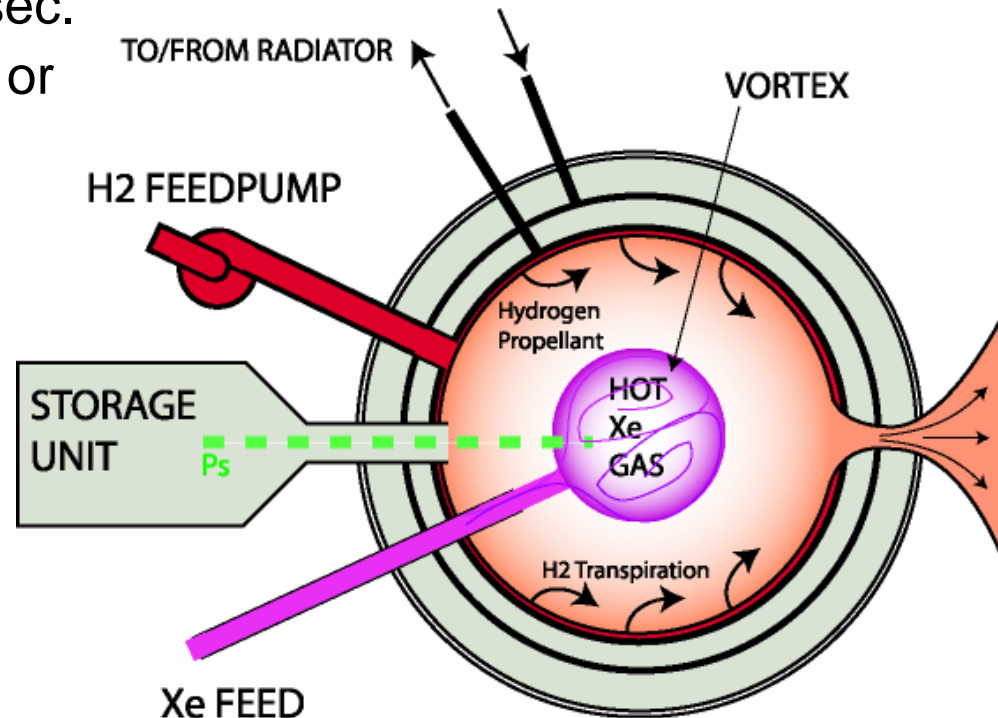
- He has a larger specific heat than Xe (5.193 vs 0.159 kJ/kg-K.)
- Xe density is larger than He (1.23 vs 40.5 kg/m³).



Gas-Core Concept

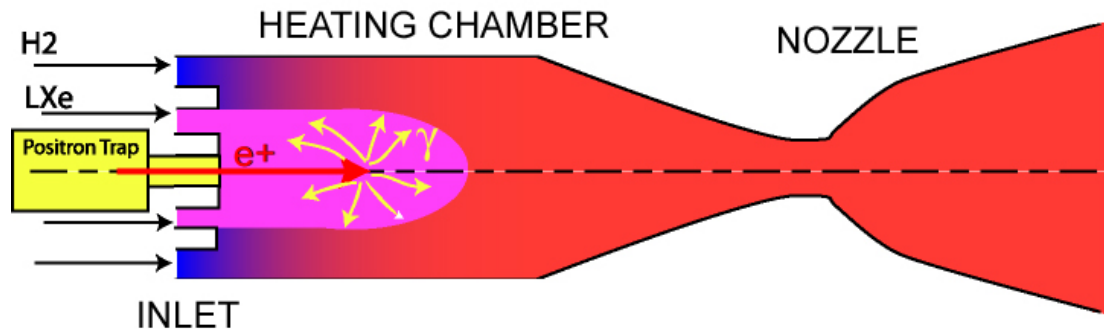
Gas-Core Rocket Should Exceed the Solid-Core's Performance and Meet Mars Mission Profile

- The theoretical maximum of e+ solid-core system Isp of 1150 sec.
- Mars mission spacecraft mass or TOF can be reduced if Isp is improved.
- Since solid-core system has proven similarities to nuclear-thermal rockets, the gas-core should meet 1150 sec.
- The gas-core should meet ~100 kN thrust requirements and have reasonable efficiency.



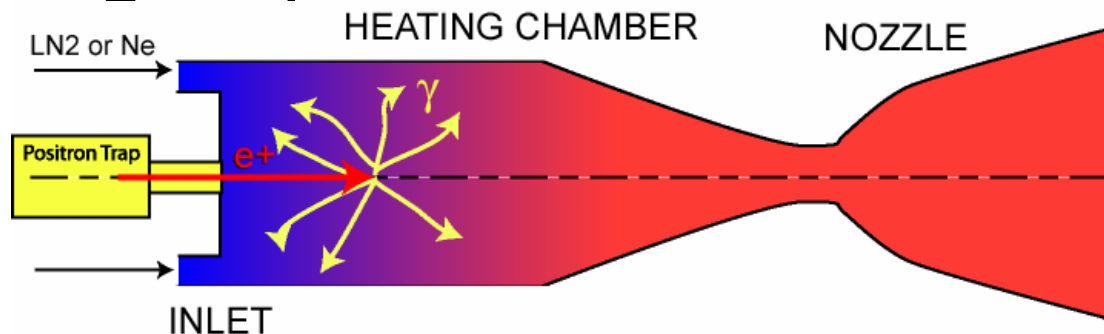
1-D and 2-D Cylindrical Simulations; Open-Cycle Gas-Core Concept may be of One or Two Species

Two species



$$u_e = \sqrt{\frac{2\gamma\bar{R}}{(\gamma-1)\bar{M}} T_c \left[1 - \left(\frac{p_e}{p_c} \right)^{(\gamma-1)/\gamma} \right]}$$

Single-species



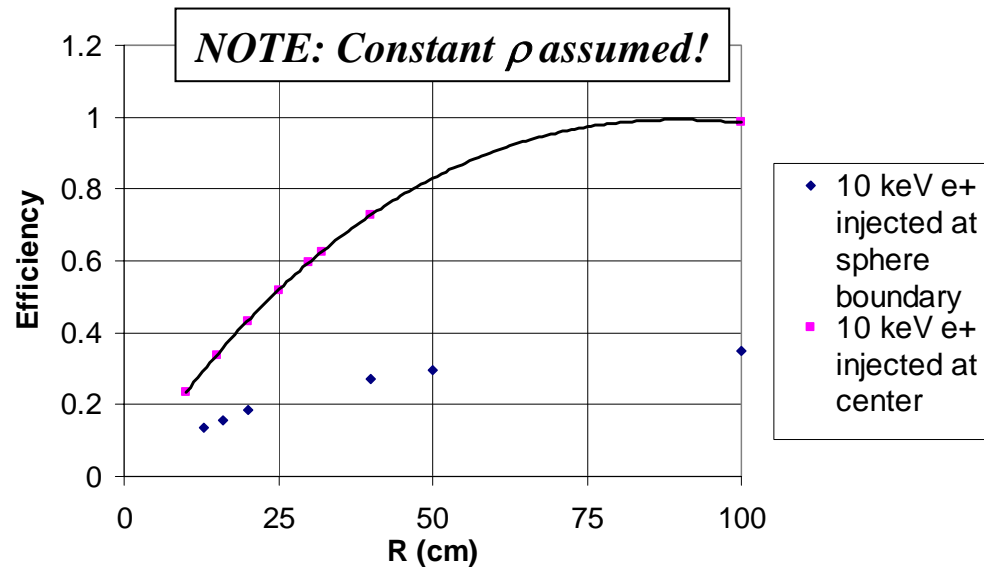
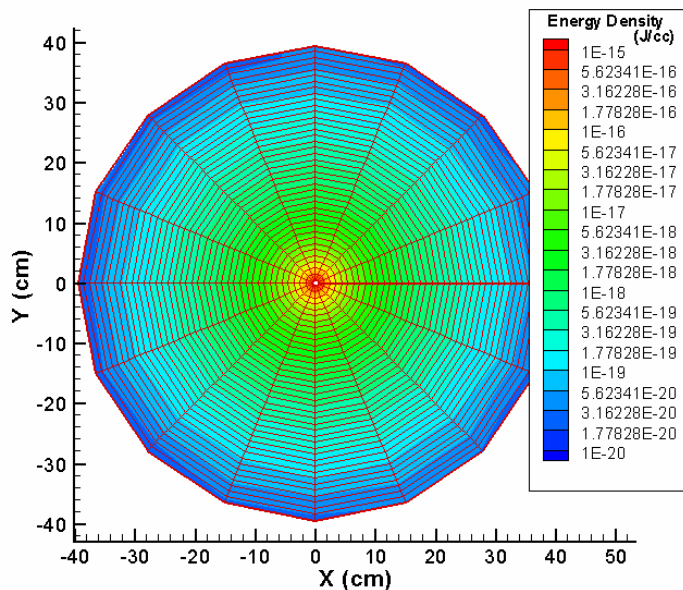
Suggests low molecular weight for high Isp, but high density needed for gamma-ray attenuation

Attenuation Simulations Provided An Approximate Radius of Engine for Single Gas

Analytically:

$$E_{\text{ABSORBED}} = E_0 (1 - \exp(-\mu \rho r))$$

- Determined that efficiency would be too low with He or H₂ (single gas/liquid) unless pressures exceeded material limits.
- Numerically used GEANT4 to get attenuation data for LN₂.
- Results show minimum of R=25 cm for >50% efficiency. Used R=40 cm. (75%). Here, gamma ray source must be located at center.



Two Codes were Used – a 1-D Euler Equation solver and a 2-D CFD commercial package (ANSWER)

SYSTEM CODE (in-house FORTRAN code)

- Assumes laminar, inviscid flow.
- Solves throat geometry.
- Provides 1-D solution as input to CFD codes.

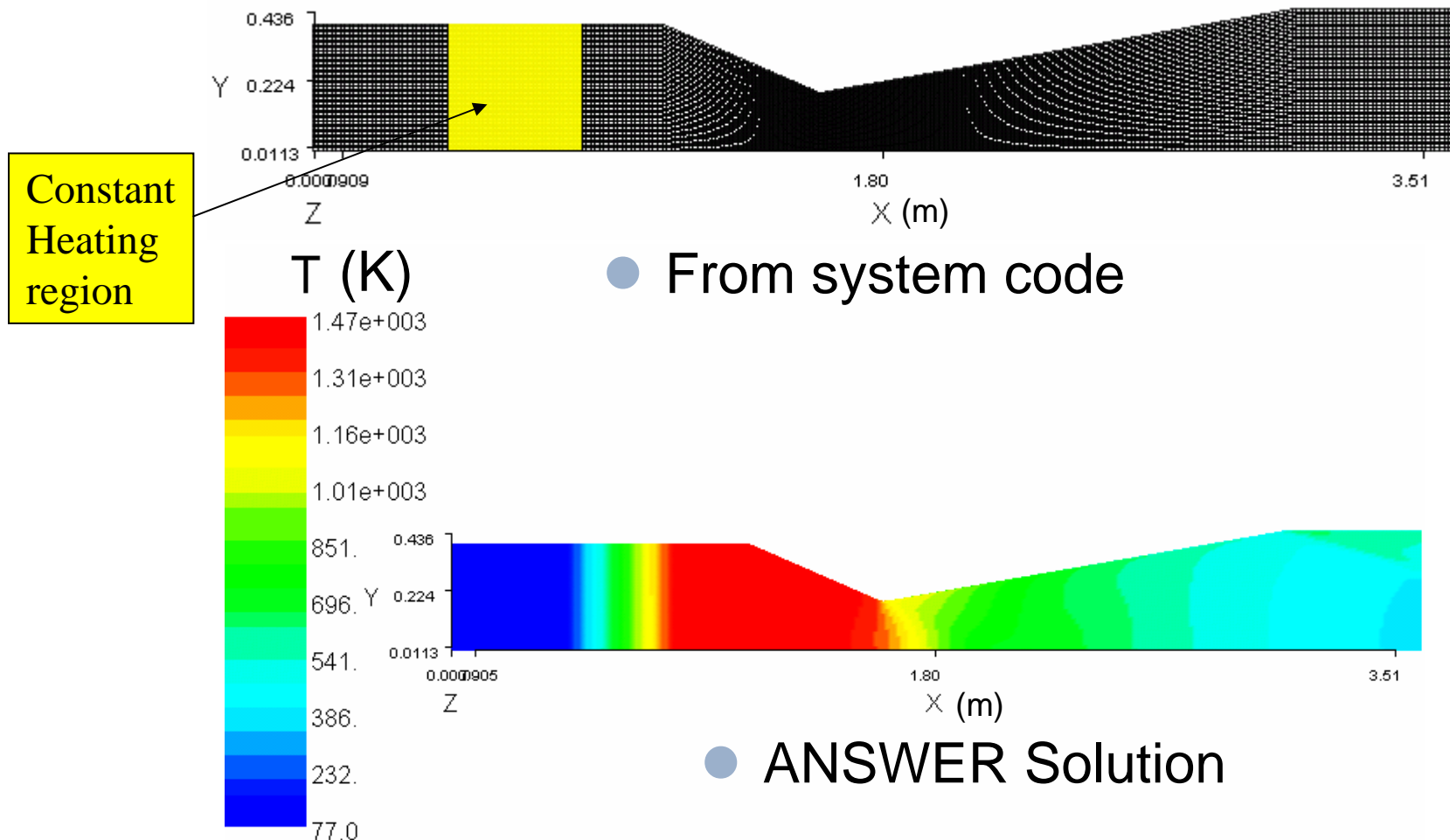
ANSWER (commercial FORTRAN, JAVA code)

- Can handle laminar, turbulent, viscous flow.
- Provides 2-D cylindrical solution.
- Includes wall effects, annular flow vortices.

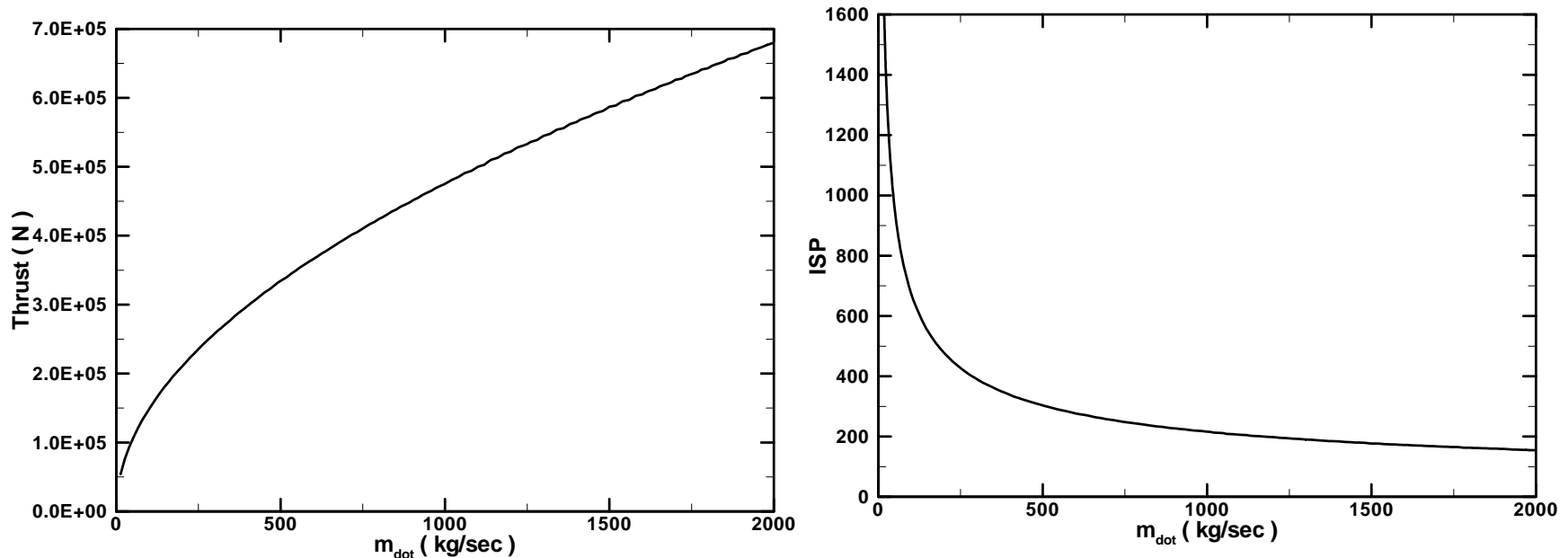
Validation

- Flow is highly turbulent but inviscid since N_2 has low viscosity.
- Tests show turbulent solution behaves laminar-like w/o diffuser at inlet, so ANSWER solution should match favorably to System Code.

Typical Mesh Generated by System Code is Directly Used in ANSWER (Single-species)



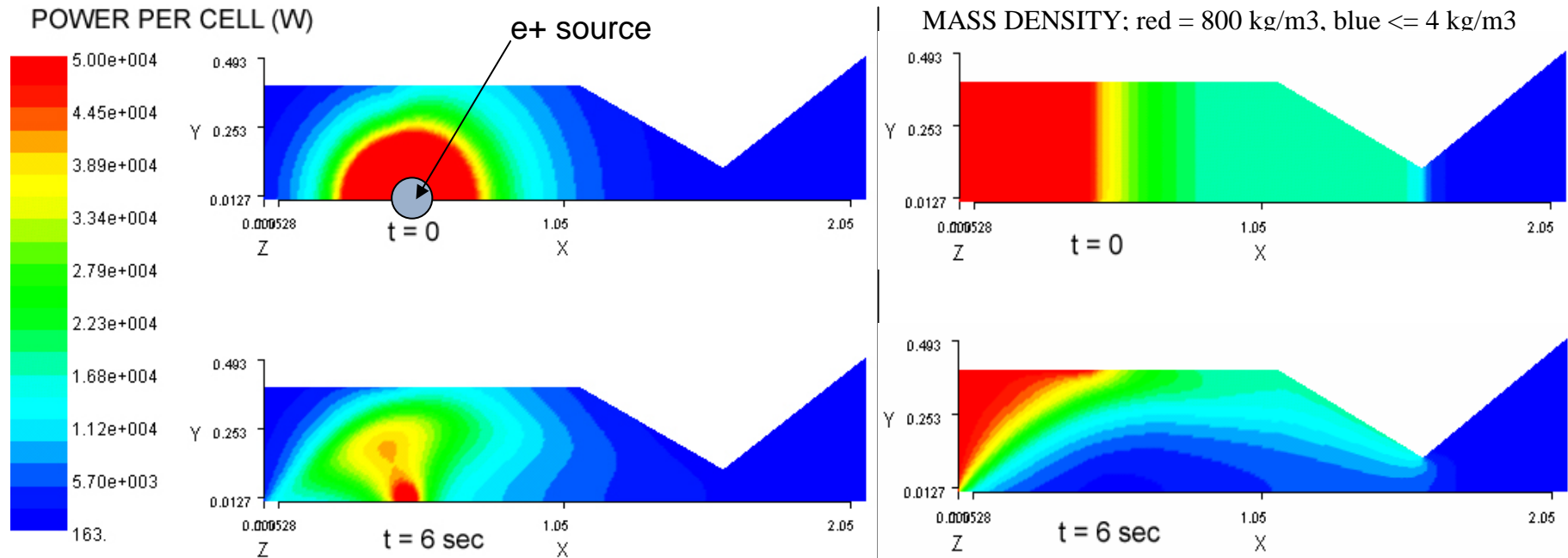
Results Using For Mars Mission (~300 MW) Show High Thrust, Low Specific Impulse with Constant Heat Density



- Values are shown for nozzle expansion ratio = 30.
- Reducing flow rate < 100 kg/sec ($T = 100$ kN) may provide >1000 sec Isp.
- But up to this point, we assumed a constant heat source. Now we address a point source with dependence of mass density:

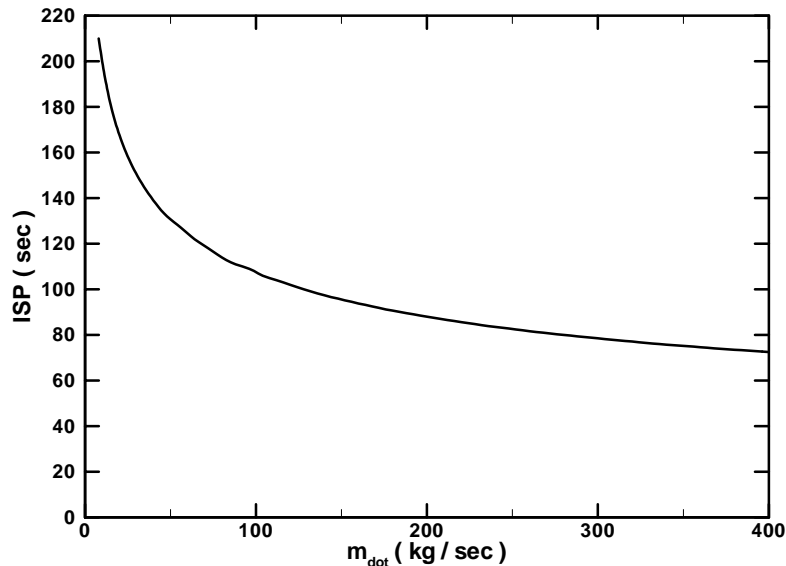
$$E_{ABSORBED} = E_0 (1 - \exp(-\mu \rho(r)r))$$

Validation of 1-D Results in 2-D CFD Code. Mass Density Interface Moves Upstream.

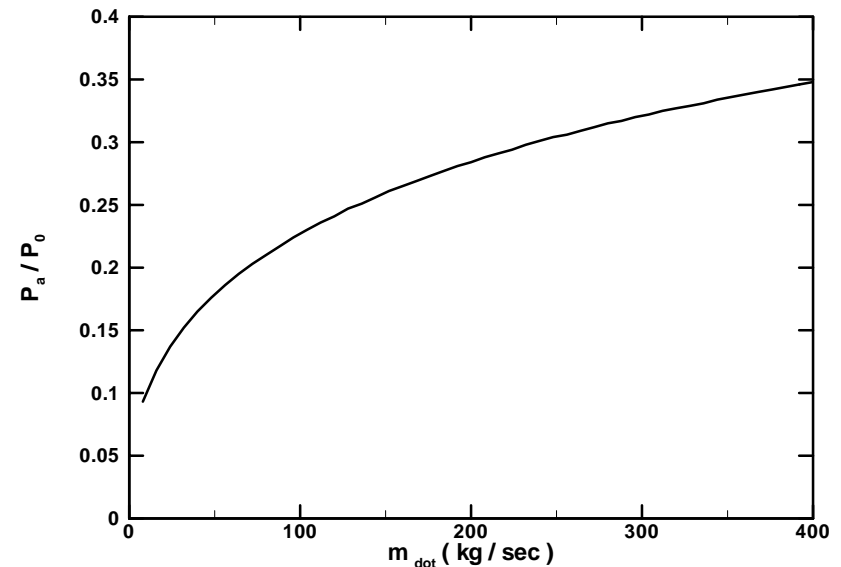
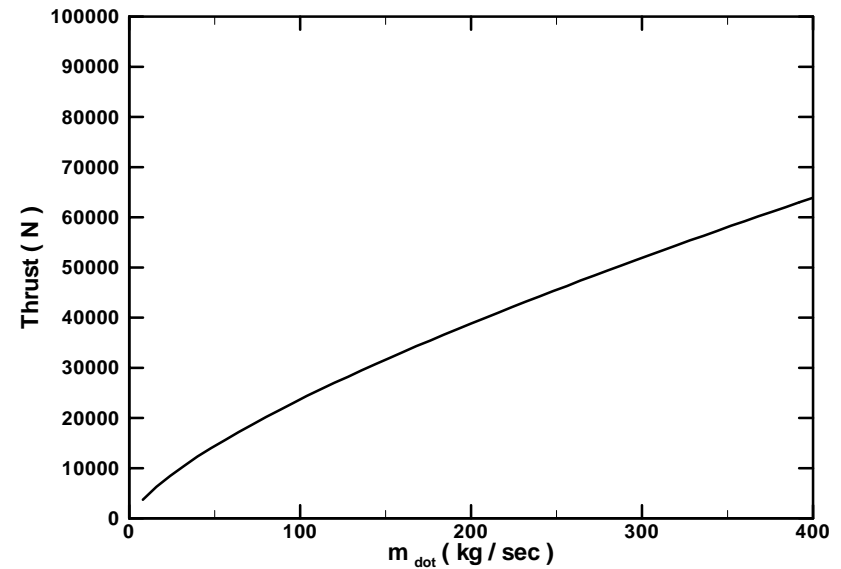


Single species (LN2)

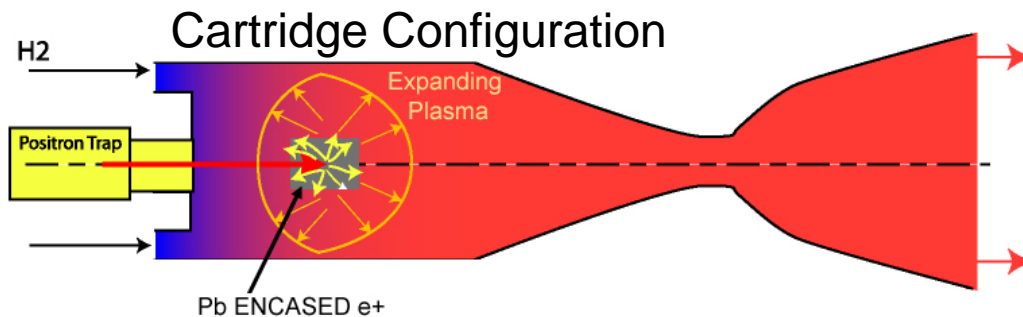
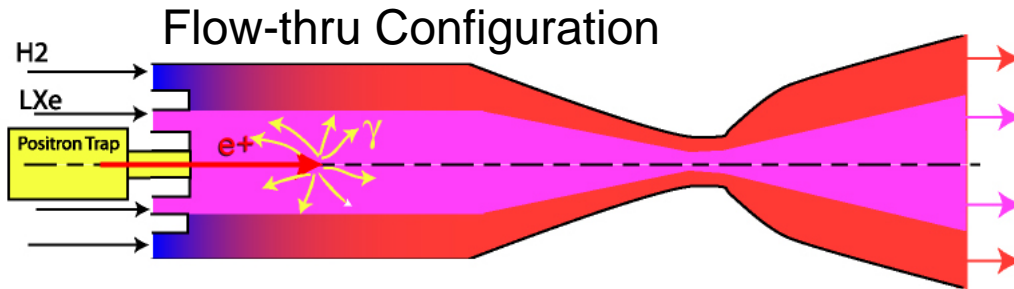
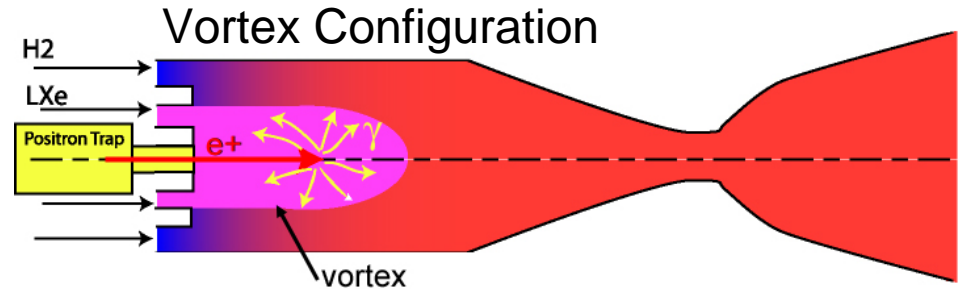
Single-species System Code Results



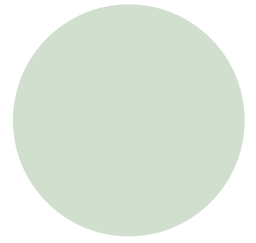
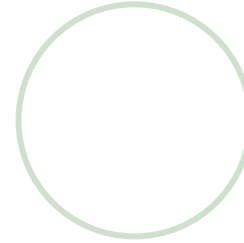
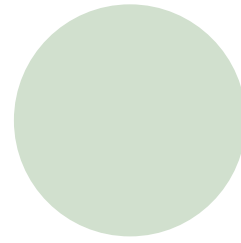
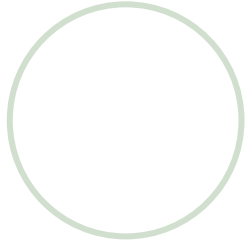
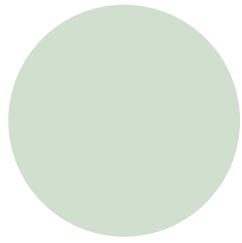
- “High” Isp (> 200 sec) only occurs with poor efficiency ($P_a/P_0 < 10\%$)
- Single-fluid concept may be infeasible since high density region moves away from energy source.



Two-Fluid Concept Variations

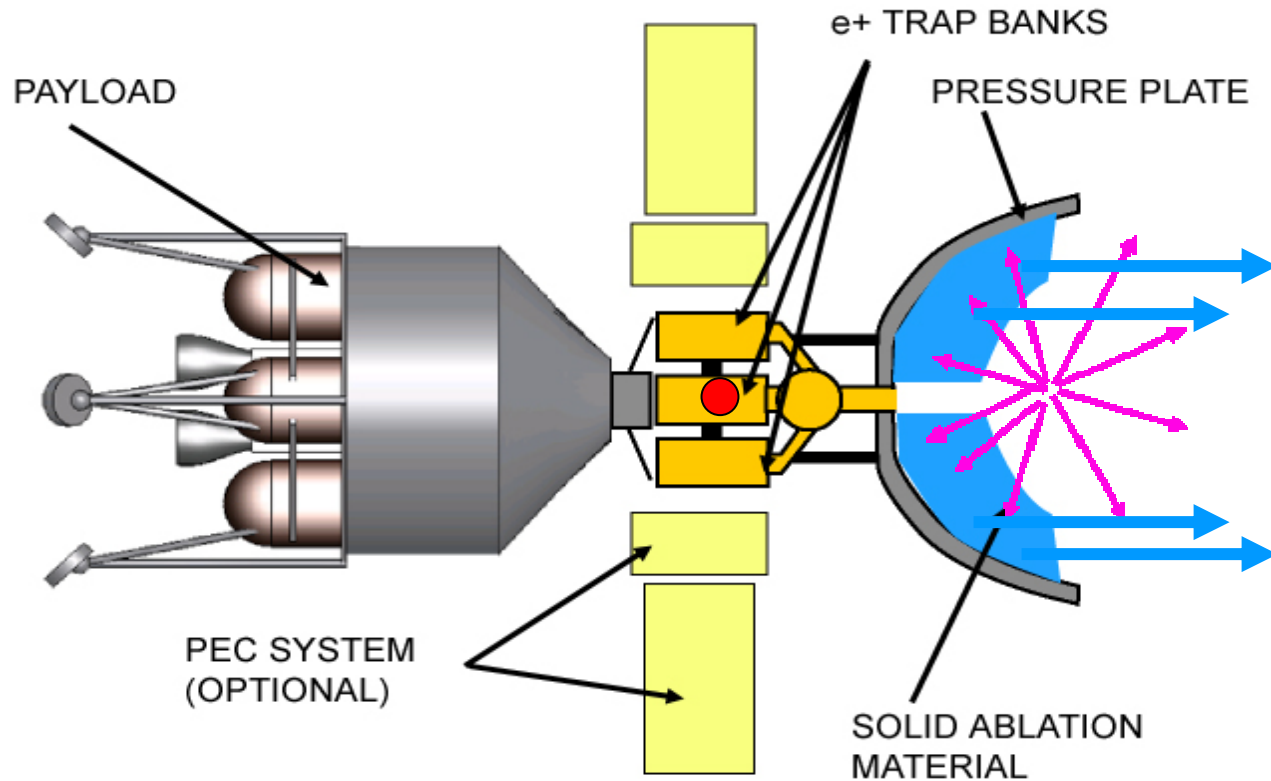


- Vortex Configuration
 - Will not work because evidence shows heating changes density profiles, causing vortex to destabilize.
- Flow-thru Configuration
 - May behave similar to single-fluid if Xe mass flow rate is significant, reducing I_{sp} .
 - Work in progress.
- Cartridge Configuration
 - e+ encased with Pb annihilate, creating plasma.
 - Lower energy photons heat H2.
 - Early studies show excellent promise with $I_{sp} = 2600$ sec, with Pb/H2 flow ratio 5:1.
 - Have to examine effects of varying mass density in system, transport to walls, pulsed behavior.



Other Concepts

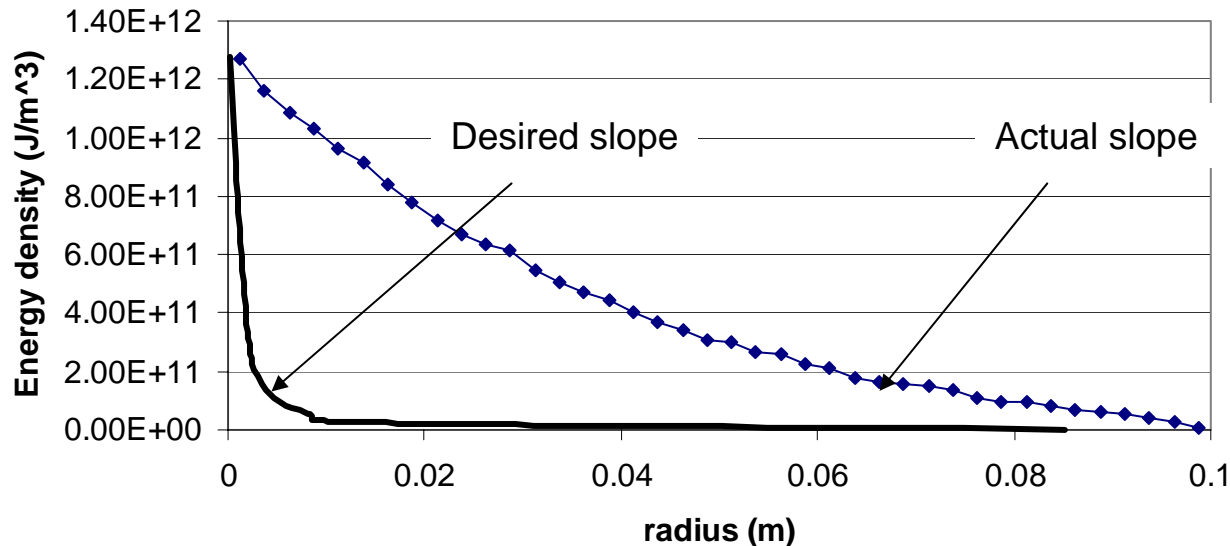
Solid Ablation Concept as a Realistic Sänger Rocket Keeps High Density Close to Positron Source



- Concept: 21st century Sanger rocket, where solid ablation material replaces unrealistic photon reflector.
- Small prompt radiation in direction of spacecraft still makes system attractive.
- Intrinsic 50% efficiency must be compared against valid gas-core concepts.

Task: Find Optimal Ablation Material and Geometry for 511 keV Gamma Rays

Heat Density Profile in 10 cm SiC using $2e22$ e+



- Minimize penetration depth to increase local energy density at surface for ablation.
- 511 keV gamma rays have long attenuation length.
- Encase e+ cartridges with lead. Lead plasma radiating at lower eV ablates solid propellant such as SiC.* Has similarity to gas-core cartridge concept.

*W. Lance Wertham, "Antiproton-Catalyzed Microfission/fusion Space Propulsion," M.S. Thesis, Dept. Aerospace Engineering, PSU, 1995.

Phase II Prospectus

- Solid Core Work:
 - A transport design/analysis effort to determine a system that will allow relatively flat radial and axial power profile.
 - Use of codes such as GEANT for attenuation studies. Material identification.
 - CFD analysis for the propulsion engine.
 - Efficiency studies of an integrated power plant with engine.
 - Experimentally design and analyze an electrically-heated heater attenuator w/ gas flow for comparison against code.
- Gas-Core Work:
 - Investigate pulsed behavior of cartridge scheme.
 - Examine wall temperature effects.
- Ablative Sänger Concept:
 - Study penetration depth of gamma rays and derive ablation material(s).
 - Investigate non-impulsive mission scenarios.

Conclusions

- Positron-based engines are “thick”.
 - “Thick” means gamma rays travel further to interact with propellant.
- Solid-Core engine will work.
 - More detailed studies required.
- Gas-core concept
 - High density gas must be kept close to high-energy gamma rays.
 - Means of reducing energies of photons to allow low-Z, high I_{sp} propellant should be investigated.
- Ablative Sänger engine promising based on previous work at Penn State.